



Data Center Design Challenges: Specifying Standby Generator Set Requirements

PowerHour webinar series for consulting engineers Experts you trust. Excellence you count on.

July 30, 2:00pm Eastern Time / 11:00am Pacific Time (1 PDH issued by Cummins Inc.)

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Meet your panelists

Cummins instructor:



Rich Scroggins Technical Advisor - Data Center Markets Cummins Inc.

Your local Cummins contacts:

- AZ, ID, NM, NV: Carl Knapp (<u>carl.knapp@cummins.com</u>)
- > CO, MT, ND, UT, WY: Christopher Scott (<u>christopher.l.scott@cummins.com</u>)
- > CA, WA, OR, AK, HI: Brian Pumphrey (brian.pumphrey@cummins.com)
- > MA, ME, NH, RI, VT: Jim Howard (james.howard@cummins.com)
- > CT, MD, NJ, NY : Charles Attisani (<u>charles.attisani@cummins.com</u>)
- > Northern IL, MI : John Kilinskis (john.a.kilinskis@cummins.com)
- NE, SD, KS: Earnest Glaser (<u>earnest.a.glaser@cummins.com</u>)
- IL, IN, KY, MO: Jeff Yates (jeffrey.yates@cummins.com)
- > IA, MO: Kirby Holden (kirby.holden@cummins.com)

Cummins facilitator:



Michael Sanford Product Strategy and Sales Enablement Leader Cummins Inc.

- > DE, MD, MN, ND, OH, PA, WI, WV: Michael Munson (michael.s.munson@cummins.com)
- TX: Scott Thomas (<u>m.scott.thomas@cummins.com</u>)
- > OK, AR: Wes Ruebman (wes.ruebman@cummins.com)
- > LA, MS, AL: Trina Casbon (trina.casbon@cummins.com)
- > TN, GA: Mariano Rojas (mariano.rojas@cummins.com)
- FL: Bob Kelly (robert.kelly@cummins.com)
- > NC, SC, VA: Bill Morris (william.morris@cummins.com)
- Canada: Ian Lindquist (<u>ian.lindquist@cummins.com</u>)

Disclaimer

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Participants are encouraged to refer to the entire text of all referenced documents. In addition, when it doubt, reach out to the Authority Having Jurisdiction.



Course Objectives

Data Center Design Challenges: Specifying Standby Generator Set Requirements

Data centers around the world have developed unique power system designs ensuring top tier reliability and cost effectiveness. In addition to their unique design, load profiles in data center applications often differ significantly from their industrial or traditional standby counterparts. In many cases, data center power systems tend to operate much closer to 1.0 power factor, even operating with a leading power factor in some instances, varying from the industry standard of specifying equipment at 0.8 lagging power factor. Additionally, data center power systems may include active power loads making load acceptance challenging for most standby generator sets as conventional methods for starting large motor loads may not be effective. Making power system design even more challenging, many loads in data centers are non-linear leading to harmonic voltage distortion. This PowerHour will explore some of the typical load characteristics that are unique to data centers and will recommend generator set specifications that may help in mitigating some of these challenges.

After completing this course, participants will be able to:

- Identify safe alternator operating zones on an alternator reactive capability chart to ensure proper operating conditions on the generator
- Recognize the differences in generator load acceptance of active power, unity power factor and conventional lagging power factor loads and define specification requirements and operating sequences for each type
- Describe the impact of non-linear loads on harmonics
- Recognize the tradeoffs in properly specifying an alternator for data center applications

What are some examples of data center power system design challenges you have encountered?









s 10



















ALTERNATOR OPERATING CHART

Leading VAR capability ~ 0.3 pu



ALTERNATOR OPERATING CHART

Leading VAR capability ~ 0.3 pu

Alternator rating is 4142 kVA 0.3*4142 = 1242 kVAR

480 V 60 Hz 1800 RPM LVSI804W Winding 12 4142 kVA 1 Per Unit 1.1 0.8 0.95 1.0 0.9 0.95 0.8 0.9 1 STATOR 0.7 0.7 0.9 ENGINE 0.8 0.6 0.7 0.6 0.6 ≷ STABILITY 0.5 0.5 Per Unit ROTOR 0.4 0.4 0.4 0.3 0.3 0.3 0.2 0.2 0.2 0.1 0.1 0.1 EXCITATION 0 -0.9 -0.8 0.9 -1 -0.7-0.4-0.3-0.2 -0. 0.2 0.3 0.4 0.5 0.6 0.7 0.8 1 -0 01 Per Unit kVar Import (Lead) Export (lag) v7

ALTERNATOR OPERATING CHART

Leading VAR capability $\sim 0.3 \text{ pu}$

Alternator rating is 4142 kVA 0.3*4142 = 1242 kVAR

3 MW genset rating @ 0.8 PF =>3750 kVA

1242/3750 = .33

Leading VAR capability = .33 pu based on genset rating



- Lower synchronous reactance (Xd) increases leading VAR capability
- Larger alternator will have lower Xd based on generator rating



ALTERNATOR OPERATING CHART

Leading VAR capability ~ 0.35 pu Alternator rating is 4464 kVA 0.35*4464 = 1562 kVAR

3 MW genset rating @ 0.8 PF =>3750 kVA genset

1562/3750 = .41

Leading VAR capability = .41 pu based on genset rating

Leading PF Takeaways



Leading PF Takeaways

Key parameter is leading VAR, not PF

 Set reverse VAR protection accordingly

Low kW, high leading VAR is a risk

- Avoid operation in this region
- Disconnect PF correction or filter caps
- Select "Gen mode" if UPS supports





Concept Check

Which of the following statements is true:

- a) A generator set's leading VAR capability can be determined from the alternator operating chart.
- b) Generator sets can operate at any power factor as long as there are power factor correction capacitors in the system.
- c) Generator sets can not operate at leading PF of less than .95.
- d) Generator sets can produce full rated output at any lagging power factor.



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UPS with Walk-In Function

Server Switched Mode Power Supplies are active loads

- Draw constant power
- As voltage drops current is increased
- V/Hz doesn't help



UPS with Walk-In Function

Server Switched Mode Power Supplies are active loads

- Draw constant power
- As voltage drops current is increased
- V/Hz doesn't help

UPS with walk-in allows gen to take on 100% active power load step

 Allows batteries to take the load initially and then ramp on to the gen









- UPS senses voltage and frequency excursion
- Transfers load to battery



- UPS senses voltage and frequency excursion
- Transfers load to battery
 - Genset voltage and frequency recover and stabilize



- UPS senses voltage and frequency excursion
- Transfers load to battery
- Genset voltage and frequency recover and stabilize
- UPS ramps load on to genset

Unity PF Transients

- Transient performance is typically documented at 0.8 PF
- Acceptance testing is typically done with resistive load banks (1.0 PF)
- Resistive loads often result in worse voltage transients than inductive loads

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Testing at 0.8 PF

- Inductance creates a lag in kW load hitting the engine
- Governor response limits frequency dip
- V/Hz voltage roll off is reduced

Transient Spec Recommendation

- Consider actual operating sequence
- Under what scenario will a 100% load acceptance be required?
 - Will this only occur in the event of a failover to a reserve gen?
 - Would a UPS walk-in function be more appropriate than a 100% load acceptance requirement?
 25 MW
 25 MW
- Specify realistic acceptance test



Transient Spec Recommendation

- Consider actual operating sequence
- Under what scenario will a 100% load acceptance be required?
 - Will this only occur in the event of a failover to a reserve gen?
 - Would a UPS walk-in function be more appropriate than a 100% load acceptance requirement?
 2.5 MW
 2.5 MW
- Specify realistic acceptance test



Spec Note Generator set manufacturer shall provide documentation from the manufacturer's sizing software demonstrating compliance with specified transient limits.



Harmonics and Non-Linear Loads





A load in which the relationship between current and voltage is directly proportional.

Load is switched on a sub-cyclic basis resulting in current that no longer conforms to the sinusoidal voltage.



Supply Type





I-THD = 29%

Switching current on a sub-cyclic basis results in a distorted current waveform

Supply Type





I-THD = 29%

Voltage Waveform

Transformer, SCR = 100



Switching current on a sub-cyclic basis results in a distorted current waveform The source (generator or utility transformer) induces current harmonic distortion on to the voltage waveform

Supply Type





I-THD = 29%

Voltage Waveform

Transformer, SCR = 100



Voltage Waveform

Genset X''_d = 12%, SCR = 8



Switching current on a sub-cyclic basis results in a distorted current waveform The source (generator or utility transformer) induces current harmonic distortion on to the voltage waveform Induced voltage harmonic distortion is proportional to source impedance (inversely proportional to short circuit ratio)



Case Study Harmonics at a Water Treatment Plant



- T1-3: 270 kVA isolation transformers, 460/460V, 5.3 Z at 170 C
- R1, R2: Line reactors, 3% Z at 60 hp
- VFD1-3: 250 hp 6 pulse PWM
- VFDTP1, VFDTP2: 60 HP, 6 pulse PWM
- MF1-3: Drive output (motor) filters
- HHP1-3: 250 HP vertical suction water pumps
- TP1, TP2: 60 HP pumps

Case Study Harmonics at a Water Treatment Plant



*Reference - Generator Loading, Harmonics Monitoring and Mitigating Analysis in a Water Treatment Plant -Eddie Jones, PE; Larry Ray, PE; Tim Shuter, PE; Square D Engineering Services

- Harmonic Voltage Distortion is a function of load generated current distortion and the source impedance
 - For a generator set source impedance is the subtransient reactance X"d
 - Harmonic distortion will be worse when running on a generator than on the utility



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 - Harmonic distortion will be worse when running on a generator than on the utility
- Harmonic distortion does not impact performance of generator sets with PMG excitation
- Use generator sizing software to select generator set that will keep harmonic distortion within acceptable limits
 - This results in an optimally sized alternator



lew UPS Load	
	Fields marked (*) are required
oad Name : * Liebert Series 610 1000 kVA UPS	
Power Requirements	Load Connections
Rated kVA : * 1000 Output V	Phase : * Single Three
	Voltage : * 480
Rectifier Details	Load Transient Limits
Rectifier Type : * 12 pulse 🗸	Max. % Voltage Dip : * 15
Harmonic Content (THDI%) : * 10	Max. % Frequency Dip : * 5
Project Level THDV% Limit : * 10	
Loading Factor	Ramp Options
Loading Factor (%) : * 100 🕕	Soft Ramp : Slow 🗸
Comments	

- Harmonic Voltage Distortion is a function of load generated current distortion and the source impedence
 - For a generator set source impedence is the subtransient reactance X"d
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ad Name 1.5 Links d Order 040 4000 M/4 UDO	Fields marked (*) are required
Device Desvicements	Lord Connections
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Spec Note Generator set manufacturer shall provide documentation from the manufacturer's sizing software demonstrating compliance with specified harmonic distortion limits.

Concept Check

Which of the following statements is false:

- a) The higher the Short Circuit Ratio, the lower the harmonics.
- b) Generator Sets and Utility handle harmonics very similarly.
- c) The lower the subtransient reactance (X"d), the lower the harmonics.
- d) An 18 pulse rectifier induces less THDI% than a 6 pulse rectifier.

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Temperature Rise

Т

	Insulation system:		Class H	l throughou	ıt		
	3 Ø Ratings	(0.8 power	factor)			60	Hz (wind
				<u>416</u> (12)	<u>440</u> (12)	<u>480</u> (12)	<u>600</u> (07)
	163° C rise ratings	@ 27° C	kW	3680	3592	3920	3920
			kVA	4600	4490	4900	4900
	150° C rise ratings	@ 40° C	kW	3304	3496	3816	3816
			kVA	4130	4370	4770	4770
<	125° C rise ratings	@ 40° C	kW	3096	3272	3571	3571
			kVA	3870	4090	4464	4464
	105° C rise ratings	@ 40° C	kW	2892	3056	3558	3338
			kVA	3615	3820	4172	4172
	80° C rise ratings	@ 40° C	kW	2512	2640	2900	2900
			kVA	3140	3300	3625	3625

Voltage Class	< 10 kV	> 10 kV
Insulation Class	Н	F
Total Temperature	180 C	160 C
Nominal Temp Rise	125 C	105 C
Nominal Ambient Temp	40 C	40 C
Hot Spot Allowance	15 C	15 C

4464 kVA is maximum load for 180 C insulation class

125 + 40 + 15 = 180

Temperature Rise

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	3 Ø Ratings (0.8 po		factor)	60 Hz (wi				
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			kVA	4130	4370	4770	4770	
0	125° C rise ratings	@ 40° C	kW	3096	3272	3571	3571	
			kVA	3870	4090	4464	4464	
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Total Temperature	180 C	160 C
Nominal Temp Rise	125 C	105 C
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Hot Spot Allowance	15 C	15 C

4464 kVA is maximum load for 180 C insulation class

125 + 40 + 15 = 180

Spec Note Specify alternator temperature rise based on insulation class and ambient conditions.

Alternator Winding Type

Random/Wire Wound



- Wire bundles
- Easier manufacturing process
- Usually better waveform quality
- Less copper and steel to reach short circuit and motor starting capabilities

Form/Bar Wound



- Individual Copper Bars
- More difficult to manufacture
- Greater mechanical strength
- Greater dielectric strength

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Spec Note Specify generator performance criteria, not manufacturing method.

Specification Requirement:

Alternator maximum subtransient reactance shall not be greater than 12%.

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3 Ø Ratings	(0.8 power factor)				60	Hz (windi
			<u>380</u> (13)	<u>416</u> (12)	<u>440</u> (12)	<u>480</u> (12)
163° C rise ratings	@ 27° C	kW	3296	3152	3336	3640
		kVA	4120	3940	4170	4550
150° C rise ratings	@ 40° C	kW	3200	3072	3248	3544
		kVA	4000	3840	4060	4430
125° C rise ratings	@ 40° C	kW	3000	2872	3040	3314
		kVA	3750	3590	3800	4142
105° C rise ratings	@ 40° C	kW	2760	2680	2840	3097
		kVA	3450	3350	3550	3871
80° C rise ratings	@ 40° C	kW	2424	2332	2468	2691
		kVA	3030	2915	3085	3364
3 Ø Reactances	5		<u>380</u>	<u>416</u>	<u>440</u>	<u>480</u>
			(13)	(12)	(12)	(12)
(Based on full load at 1	25° C rise ratin	ig)				\frown
Synchronous			2.700	3.120	2.948	2.700
Transient			0.193	0.220	0.208	0.101
Subtransient			0.142	0.161	0.152	0.140
Negative sequence			0.205	0.233	0.221	0.202
Zero sequence			0.027	0.031	0.029	0.027

Reactances at genset rating (3750 kVA) Synchronous = 2.4 pu Subtransient = .126 pu

Specification Requirement:

Alternator maximum subtransient reactance shall not be greater than 12%.

Should an oversized alternator be selected?

An oversized alternator may have...

- Better harmonic performance
- Greater leading VAR capability
- Lower subtransient reactance

3 Ø Ratings	(0.8 power factor)				60	Hz (windi
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An oversized alternator may also have...

- Higher fault current
- Slower start time
- and may be more expensive!

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Course Summary

Data Center Design Challenges: Specifying Standby Generator Set Requirements

- Identify safe alternator operating zones on an alternator reactive capability chart to ensure proper operating conditions on the generator
- Recognize the differences in generator load acceptance of active power, unity power factor and conventional lagging power factor loads and define specification requirements and operating sequences for each type
- Describe the impact of non-linear loads on harmonics
- Recognize the tradeoffs in properly specifying an alternator for data center applications

Recommendations

- Define the generator's leading VAR requirements and identify the generator's leading VAR capabilities. Specify
 alternator and operating sequences accordingly
- Consider UPS walk-in function rather than oversizing generator set for full load acceptance
- Specify transient requirements and acceptance test requirements that are representative of actual usage
- Use generator set sizing software to evaluate harmonic requirements

Additional Resources

Cummins White Papers

- Data Center Continuous (DCC) Ratings: A Comparison of DCC Ratings, ISO Definitions and Uptime Requirements (Nov 2019)
- Understanding ISO 8528-1 Generator Set Ratings (Nov 2019)
- Transient Performance of Generating Sets
- Specifying and Validating Motor Starting Capability

Cummins On-Demand Webinars

- Generator Set Ratings for Data Centers and Other Applications
- Common Failure Modes of Data Center Back Up Power Systems
- Using Fuel Cells to Address Energy Growth and Sustainability Challenges in Data Centers
- Advanced Generator Set Sizing Software: Transient Performance and Motor Load

BULLETIN SE00405 | TECHNICAL INFORMATION FROM CUMMIN DATA CENTER CONTINUOUS RATINGS

White Paper By David Matuseski

DATA CENTER CONTINUOUS (DCC) RATINGS: A COMPARISON OF DCC RATINGS, ISO DEFINITIONS AND UPTIME REQUIREMENTS

While Uptime Institute references the ISO8528-1 definitions for generator ratings in their publication Tier Standard: Topology, they do not require the use of these definitions for generators to meet the Tier III and Tier IV requirements, as described in the same publication. A more cost-effective and reliable generator rating that meets the Tier III and Tier IV requirements can be achieved when the generator manufacturer develops ratings specifically for data center applications.

DIESEL GENERATORS IN A TIER III OR TIER IV SYSTEM

In Tier III and Tier IV systems, Uptime Institute defines the diesel generators as the primary source of power and the utility as an economic alternative. This definition puts two important requirements on the diesel generators. First, they must be large enough to carry the entire data center load. Second, there can be no limit on the number of hours the diesel generators can run.



Figure 1 – Cummins QSK95-based generator sets offering ratings up to 3.5 MW based on ISO 8528-1.

Cummins

Q&A

Please type your questions, comments and feedback in the **Zoom Q&A** window.

After the PowerHour, a complete list of questions and answers will be published on powersuite.cummins.com.



Rich Scroggins Technical Advisor - Data Center Markets Cummins Inc.

Your local Cummins contacts:

- > AZ, ID, NM, NV: Carl Knapp (carl.knapp@cummins.com)
- > CO, MT, ND, UT, WY: Christopher Scott (<u>christopher.l.scott@cummins.com</u>)
- > CA, WA, OR, AK, HI: Brian Pumphrey (<u>brian.pumphrey@cummins.com</u>)
- > MA, ME, NH, RI, VT: Jim Howard (james.howard@cummins.com)
- > CT, MD, NJ, NY : Charles Attisani (charles.attisani@cummins.com)
- Northern IL, MI : John Kilinskis (john.a.kilinskis@cummins.com)
- NE, SD, KS: Earnest Glaser (<u>earnest.a.glaser@cummins.com</u>)
- IL, IN, KY, MO: Jeff Yates (jeffrey.yates@cummins.com)
- > IA, MO: Kirby Holden (kirby.holden@cummins.com)



Michael Sanford Product Strategy and Sales Enablement Leader Cummins Inc.

- > DE, MD, MN, ND, OH, PA, WI, WV: Michael Munson (michael.s.munson@cummins.com)
- TX: Scott Thomas (<u>m.scott.thomas@cummins.com</u>)
- > OK, AR: Wes Ruebman (wes.ruebman@cummins.com)
- LA, MS, AL: Trina Casbon (trina.casbon@cummins.com)
- > TN, GA: Mariano Rojas (mariano.rojas@cummins.com)
- FL: Bob Kelly (<u>robert.kelly@cummins.com</u>)
- NC, SC, VA: Bill Morris (<u>william.morris@cummins.com</u>)
- Canada: Ian Lindquist (<u>ian.lindquist@cummins.com</u>)

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Please complete the brief survey before exiting the webinar!



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- > AZ, ID, NM, NV: Carl Knapp (carl.knapp@cummins.com)
- > CO, MT, ND, UT, WY: Christopher Scott (<u>christopher.l.scott@cummins.com</u>)
- > CA, WA, OR, AK, HI: Brian Pumphrey (<u>brian.pumphrey@cummins.com</u>)
- > MA, ME, NH, RI, VT: Jim Howard (james.howard@cummins.com)
- > CT, MD, NJ, NY : Charles Attisani (charles.attisani@cummins.com)
- Northern IL, MI : John Kilinskis (john.a.kilinskis@cummins.com)
- NE, SD, KS: Earnest Glaser (<u>earnest.a.glaser@cummins.com</u>)
- IL, IN, KY, MO: Jeff Yates (jeffrey.yates@cummins.com)
- > IA, MO: Kirby Holden (kirby.holden@cummins.com)



Michael Sanford Product Strategy and Sales Enablement Leader Cummins Inc.

- > DE, MD, MN, ND, OH, PA, WI, WV: Michael Munson (michael.s.munson@cummins.com)
- > TX: Scott Thomas (m.scott.thomas@cummins.com)
- > OK, AR: Wes Ruebman (wes.ruebman@cummins.com)
- LA, MS, AL: Trina Casbon (trina.casbon@cummins.com)
- > TN, GA: Mariano Rojas (mariano.rojas@cummins.com)
- FL: Bob Kelly (<u>robert.kelly@cummins.com</u>)
- NC, SC, VA: Bill Morris (<u>william.morris@cummins.com</u>)
- Canada: Ian Lindquist (<u>ian.lindquist@cummins.com</u>)

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